时滞反馈力作用下含有分数阶阻尼的随机系统的 响应与分叉研究*

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摘要 分析了时滞反馈力作用下含有分数阶阻尼的随机系统,并讨论了该系统的稳态响应及随机分叉.首先,通过对含有时滞项的近似处理以及基于广义谐和函数的随机平均法得到了该系统的稳态响应. 然后使用算例对方法的有效性进行了验证,其中主要研究了时滞反馈作用力和分数阶阻尼对系统稳态响应的影响,结果表明上述两者的变化会影响系统的稳态响应并引发随机分叉现象.

关键词 时滞, 分数阶, 随机系统, 随机平均法, 随机分叉

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引言

分数阶微积分是一个古老而又新鲜的概念,它 的研究历史几乎与整数阶同步[1,2]. 三百多年前就 曾被数学家们提出,之后许多著名科学家就分数阶 微积分理论展开了广泛的讨论,并给出了合理的定 义. 由于分数阶微积分没有整数阶在某些应用中的 局限性,可以很好地被用来描述具有非局域性和历 史依赖性的材料或系统的性态. 近几十年来,分数 阶微积分得到了广泛发展,同时含有分数阶微积分 的随机系统也被一些学者所关注. Bagely 和 Torvik[3-5]总结了大量前人工作并用实验证明了利用 分数阶本构关系可以很好地描述粘弹性材料的应 力松弛和蠕变现象, Metzle 和 Klafter^[6]利用分数阶 来研究反常扩散, Agrawal [7,8] 得到了含分数阶阻尼 系统的单自由度系统的随机响应, Spanos 和 Zedin^[9]用频域方法研究了含有分数阶的动力系统的 随机振动, Huang 和 Jin[10] 利用随机平均法研究了 含有分数阶的强非线性系统的随机响应和稳定性, Chen 和 Zhu^[11-13]研究了不同噪声激励下的分数阶 随机系统.

在现实中,很多领域都存在时滞现象,如物理 学、经济学、控制等,有着广泛的实际工程背景,特 别是在控制中,时滞往往会导致系统性能的改变.目前,分数阶控制系统也被不少学者所关注,但很多学者已经研究了确定性情况下的时滞系统,对于含有时滞因素的随机系统研究较少. Guilouzic [14]等用小时滞近似法得到了随机时滞微分方程的稳态概率密度,Frank 和 Beek [15]得到了线性随机时滞微分方程的平稳解,Liu 和 Zhu [16] 用随机平均法得到了具时滞反馈控制力的拟可积 Hamilton 系统响应的稳态概率密度. 但是大部分的研究都是基于整数阶完成的.

本文首先对时滞项进行近似处理,并利用基于 广义谐和函数的随机平均法,得到了具有分数阶导 数阻尼的单自由度非线性随机系统的响应.同时进 行数值模拟并对结果进行了讨论.

1 时滞反馈力作用下含有分数阶阻尼的随机系统

本文考虑一个具时滞反馈控制力的单自由度 非线性随机系统,该系统中含有分数阶阻尼,其运 动方程为:

$$\ddot{x} + \varepsilon \gamma(x, \dot{x}) \dot{x} + \varepsilon c D^{\alpha} x(t) + g(x) + \varepsilon F(x_{\tau}, \dot{x}_{\tau})$$

$$= \varepsilon^{\frac{1}{2}} f_{k}(x, \dot{x}) W_{k}(t)$$

$$0 < \alpha < 1, \ k = 1, 2, \dots m$$

$$(1)$$

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其中 ε 是一个正的小参数; $\varepsilon \gamma(x,\dot{x})\dot{x}$ 为线性或非 线性阻尼, $\varepsilon cD^{\alpha}x(t)$ 是分数阶阻尼项; g(x) 为线性 和(或)非线性刚度,是关于广义位移x的奇函数; $\varepsilon F(x_{\tau},\dot{x}_{\tau})$ 为时滞反馈力; $W_{k}(t)$ 是强度为 $2D_{kl}$ 的高 斯白噪声.

对于分数阶阻尼项 $\varepsilon cD^{\alpha}x(t)$,这里采用分数 阶的 Riemann-Liouville 定义:

$$D^{\alpha}f(t) = \frac{1}{\Gamma(1-\alpha)} \frac{d}{dt} \int_{0}^{t} \frac{f(t-\tau)}{\tau^{\alpha}} d\tau,$$

$$0 < \alpha < 1$$
(2)

时滞反馈力

由于 ε 是一个小参数,使用广义谐和函数,假 设系统在平衡点周围有周期解族[17]:

$$x(t) = A\cos\Theta(t) \tag{3a}$$

$$\dot{x}(t) = -Av(A, \Theta)\sin\Theta(t)$$
 (3b)

$$\Theta(t) = \Phi(t) + \Gamma(t) \tag{3c}$$

其中,

$$v(A,\Theta) = \frac{d\Phi}{dt} = \sqrt{\frac{2[U(A) - U(A\cos\Theta)]}{A^2\sin^2\Theta}}$$
$$= b_0(A) + \sum_{r=1}^{\infty} b_r(A)\cos r\Theta \tag{4}$$

U(x) 为系统势能.

由方程(4)得到系统的平均频率 $\omega(A)$:

$$\omega(A) = \frac{1}{2\pi} \int_0^{2\pi} v(A, \Theta) d\Theta = b_0(A)$$
 (5)

将平均频率 $\omega(A)$ 带入方程(3c),可得到:

$$\Theta(t) \approx \omega(A)t + \Gamma(t) \tag{6}$$

由于振幅 A 和相位 Γ 是慢变过程,可以得到:

$$A(t - \tau) \approx A(t) \tag{7b}$$

$$\Gamma(t-\tau) \approx \Gamma(t)$$
 (7c)

将方程(7)带入方程(3),则有:

 $\Theta(t-\tau) \approx \Theta(t) - \omega(A)\tau$

$$x(t-\tau) = A(t-\tau)\cos\Theta(t-\tau)$$

$$\approx A(t)\cos(\Theta(t) - \omega(A)\tau)$$

$$\approx x(t)\cos\omega(A)\tau - \frac{\dot{x}(t)}{\omega(A)}\sin\omega(A)\tau \quad (8)$$

$$\begin{split} \dot{x}(t-\tau) &= -A(t-\tau) \frac{\mathrm{d}\Phi(t-\tau)}{\mathrm{d}t} \mathrm{sin}\Theta(t-\tau) \\ &\approx -A(t)\omega(A) \mathrm{sin}(\Theta(t) - \omega(A)\tau) \\ &\approx \dot{x}(t) \mathrm{cos}\omega(A)\tau + x(t)\omega(A) \mathrm{sin}\omega(A)\tau \end{split}$$

故时滞反馈力可以近似地表达为:

 $F(x_{\tau}, \dot{x}_{\tau}) = F_1(x, \tau) + F_2(x, \dot{x}, \tau) \dot{x}(t)$ (10)因此,系统(1)可转化为下列近似系统:

$$\ddot{x} + \varepsilon c D^{\alpha} x(t) + \varepsilon (\gamma + F_2) \dot{x}(t) + g(x) + \varepsilon F_1$$

$$= \varepsilon^{\frac{1}{2}} f_{\nu}(x, \dot{x}) W_{\nu}(t) \tag{11}$$

令 $\gamma + F_2 = c_1, g(x) + \varepsilon F_1 = G(x)$,方程(11)可写 作:

$$\ddot{x} + \varepsilon c D^{\alpha} x(t) + \varepsilon c_1 \dot{x}(t) + G(x) = \varepsilon^{\frac{1}{2}} f_k(x, \dot{x}) W_k(t)$$
(12)

故原式系统(1)可以近似表达为不含时滞反馈力 的系统(12).

随机平均法 3

对于近似系统 (12), 系统势能 U(x)为:

$$U(x) = \int_0^x G(u) \, \mathrm{d}u \tag{13}$$

由(3)、(4)可推得:

$$\frac{\mathrm{d}A}{\mathrm{d}t} = \varepsilon F'_{1}(A,\Gamma) + \varepsilon^{\frac{1}{2}} G_{1k}(A,\Gamma) W_{k}(t) \qquad (14a)$$

$$\frac{\mathrm{d}\Gamma}{\mathrm{d}t} = \varepsilon F'_{2}(A,\Gamma) + \varepsilon^{\frac{1}{2}} G_{2k}(A,\Gamma) W_{k}(t) \quad (14b)$$

其中,

(7a)

(9)

$$F'_{1}(A,\Gamma) = F'_{11} + F'_{12} \tag{15a}$$

$$F'_{11} = \frac{Av\sin\Theta}{G(A)}cD^{\alpha}(A\cos\Theta)$$
 (15b)

$$F'_{12} = -\frac{A^2 v^2 \sin^2 \Theta}{G(A)} c_1 \tag{15c}$$

$$F'_{2}(A,\Gamma) = \frac{v \cos\Theta}{G(A)} c D^{\alpha}(A \cos\Theta) - \frac{Av^{2} \sin\Theta \cos\Theta}{G(A)} c_{1}$$

(15d)

$$G_{1k} = \frac{-Av\sin\Theta}{G(A)} f_k \tag{15e}$$

$$G_{2k} = \frac{-v\cos\Theta}{G(A)} f_k \tag{15f}$$

根据 Stratonovich-Khasminskii 定理^[18], 当 $\varepsilon \rightarrow 0$ 时,A 为一维扩散过程,其平均 Itô 方程为:

$$dA = m(A) dt + \sigma(A) dB(t)$$
 (16)

其中漂移系数与扩散系数分别为:

$$m(A) = \varepsilon \langle F'_1 + D_{kl} \frac{\partial G_{1k}}{\partial A} G_{1l} + D_{kl} \frac{\partial G_{1k}}{\partial \Gamma} G_{2l} \rangle_{\Theta} \quad (17a)$$

$$\sigma(A) = \varepsilon < 2D_{kl}G_{1k}G_{1l} > \Theta$$
 (17b)

上式中 < ● > a表示对 @ 的平均.

为求得漂移系数和扩散系数,可通过对 Θ 的 Fourier 级数展开得到,而对于其中含分数阶项 F'11,有:

$$F'_{11} = \frac{Av\sin\Theta}{G(A)}D^{\alpha}(A\cos\Theta)$$

$$< F'_{11} >_{\Theta} = \frac{1}{G(A)} \lim_{T \to \infty} \frac{1}{T} \int_{0}^{T} D^{\alpha}(A\cos\Theta) \times Av\sin\Theta dt$$

$$= \frac{1}{G(A)} \lim_{T \to \infty} \frac{1}{T\Gamma(1-\alpha)} \int_{0}^{T} Av\sin\Theta \times \left(\frac{d}{dt} \int_{0}^{t} \frac{x(t-\tau)}{\tau^{\alpha}} d\tau\right) dt$$

$$= \frac{1}{G(A)\Gamma(1-\alpha)} \lim_{T \to \infty} \frac{1}{T} \int_{0}^{T} Av\sin\Theta \times d\left(\int_{0}^{t} \frac{x(t-\tau)}{\tau^{\alpha}} d\tau\right)$$

$$= \frac{1}{G(A)\Gamma(1-\alpha)} \lim_{T \to \infty} \left\{\frac{1}{T}(Av\sin\Theta \times \int_{0}^{t} \frac{x(t-\tau)}{\tau^{\alpha}} d\tau\right) \Big|_{0}^{T} - \frac{1}{T} \int_{0}^{T} \left(\int_{0}^{t} \frac{x(t-\tau)}{\tau^{\alpha}} d\tau\right) \frac{d}{dt} Av\sin\Theta dt\right\}$$

$$\approx \frac{-1}{G(A)\Gamma(1-\alpha)} \lim_{T \to \infty} \frac{1}{T} \int_{0}^{T} AG(A\cos\Theta)$$

$$\left[\cos\Theta \int_{0}^{t} \frac{\cos\omega(A)\tau}{\tau^{\alpha}} d\tau + \sin\Theta \int_{0}^{t} \frac{\sin\omega(A)\tau}{\tau^{\alpha}} d\tau\right] dt \qquad (18)$$

当 t 比较大时下述积分可渐进展开为:

$$\int_{0}^{t} \frac{\cos(\omega \tau)}{\tau^{q}} d\tau = \omega^{(q-1)} \int_{0}^{s} \frac{\cos(u)}{u^{q}} du$$

$$= \omega^{(q-1)} \left[\Gamma(1-q) \sin(\frac{q\pi}{2}) + \frac{\sin(s)}{s^{q}} + O(s^{(-q-1)}) \right]$$

$$\int_{0}^{t} \frac{\sin(\omega \tau)}{\tau^{q}} d\tau = \omega^{(q-1)} \int_{0}^{s} \frac{\sin(u)}{u^{q}} du$$

$$= \omega^{(q-1)} \left[\Gamma(1-q) \cos(\frac{q\pi}{2}) + \frac{\cos(s)}{s^{q}} + O(s^{(-q-1)}) \right]$$

$$u = \omega \tau, s = \omega t$$
(19)

将上式带入(18)式,可简化为:

$$\langle F_{11} \rangle_{\Theta} = \frac{-A}{G(A)} \times \frac{1}{2\pi\omega^{1-\alpha}} \int_{0}^{2\pi} G(A\cos\Theta)$$

$$\left[\cos\Theta\sin(\frac{q\pi}{2}) + \sin\Theta\cos(\frac{q\pi}{2})\right] d\Theta$$

(20)

故,与(16)对应的 Fokker-Planck-Kolmogorov

(FPK)方程为:

$$\frac{\partial p}{\partial t} = -\frac{\partial}{\partial A} \left[m(A)p \right] + \frac{1}{2} \frac{\partial^2}{\partial A^2} \left[\sigma^2(A)p \right]$$
 (21)

取边界条件为:

$$p =$$
 有限 $A =$ 0 , (22a)

$$p, \frac{\partial p}{\partial A} \rightarrow 0 \quad A \rightarrow \infty$$
 (22b)

则平稳解为:

$$p(A) = \frac{C}{\sigma^2(A)} \exp\left[\int_0^A \frac{2m(u)}{\sigma^2(u)} du\right]$$
 (23)

其中 C 是归一化常数,

系统 Hamilton 函数 H = U(A) 的平稳概率密度为:

$$p(H) = p(A) \left| \frac{dA}{dH} \right| = \frac{p(A)}{G(A)} \Big|_{A = U^{-1}(H)}$$
 (24)

其中 U^{-1} 是 U 的反函数. 位移与速度的联合密度为:

$$p(x,\dot{x}) = \frac{p(H)}{T(H)} \bigg|_{H = \frac{x^2}{2} + U(x)}$$
 (25)

其中,

$$T(H) = \frac{2\pi}{\omega(A)} \bigg|_{A = U^{-1}(H)}$$
 (26)

4 算例

算例1

考虑 Gauss 白噪声激励下具有线性时滞反馈 控制力的系统,其运动方程可表示为:

 $\ddot{x} + cD^{\alpha}x(t) + \omega_0^2x + (a_1x_{\tau} + a_2\dot{x}_{\tau}) = W(t)$ (27) 其中 c 是分数阶阻尼项的系数,W(t) 是强度为 2D 的高斯白噪声. 使用上节中近似方法,系统可化为不含时滞项的系统:

$$\ddot{x} + cD^{\alpha}x(t) + \beta\dot{x}(t) + \omega^{2}x = W(t)$$

$$\text{ i.t.}$$

$$\beta = a_2 \cos \omega_0 \tau - \frac{a_1}{\omega_0} \sin \omega_0 \tau \tag{29a}$$

$$\omega^2 = \omega_0^2 + a_1 \cos \omega_0 \tau + a_2 \omega_0 \sin \omega_0 \tau \tag{29b}$$

应用变换:

$$x(t) = A\cos\Theta(t), \dot{x}(t) = -A\omega\sin\Theta(t)$$

$$\Theta(t) = \omega t + \Gamma(t), G(x) = \omega^{2}x$$
(30)

根据随机平均法,平均 Itô 方程为 (16),漂移与扩散系数分别为:

$$m(A) = -\frac{c\sin(\frac{\alpha\pi}{2})A}{2\omega^{1-\alpha}} - \frac{\beta A}{2} + \frac{D}{2\omega^2 A}$$
(31a)

$$\sigma^2(A) = \frac{D}{\omega^2} \tag{31b}$$

该系统平稳解为:

$$p(A) = \frac{C\omega^2 A}{D} \exp\left[-\frac{c\sin(\frac{\alpha\pi}{2})\omega^{1+\alpha}}{2D}A^2 - \frac{\beta\omega^2}{2D}A^2\right]$$
(32)

根据(32)式可导出关于位移速度的联合概率 密度、关于位移的概率密度以及关于速度的概率密 度.

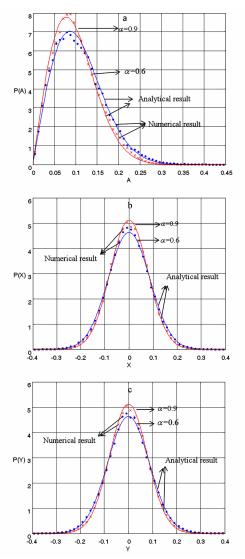


图1 当α改变时的稳态概率密度

Fig. 1 Stationary probability density with different values of α

为了验证上述结果的有效性,利用 Monte-Carlo 方法对系统进行数值模拟. 从图中可看到数值结果与解析结果基本吻合,证明了解析方法的有效性. 这里先不考虑时滞反馈力的影响. 首先讨论当参数α变化时对系统响应的影响(见图 1). 取系统参数

为 c=0.1, D=0.0006, $\omega_0=1.0$. 从图 1(a) 可以看到,随着参数 α 的增大概率密度曲线的峰值增大并向零点处靠近,从图 1(b), 1(c) 可以看到: 概率密度曲线的峰值出现在零点位置,并随着 α 的增大,曲线的峰值在零点处越高,这说明系统越趋向于稳定在零点位置.

图 2 为当时滞反馈力发生改变时系统的概率密度图. 其中参数为 c=0.1, $\alpha=0.6$, D=0.006, $\omega_0=1.0$, $a_1=0.1$, $a_2=0$. 可以看到:随着 τ 的变化, 概率密度曲线的峰值大小也发生了改变, 这说明时滞反馈力对系统的响应造成了影响.

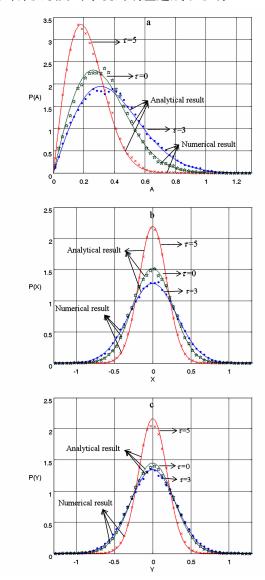


图 2 当 τ 改变时的稳态概率密度

Fig. 2 Stationary probability density with different values of τ

算例 2

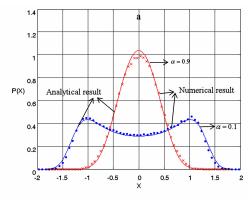
考虑含有分数阶阻尼项的非线性系统,系统方程如下:

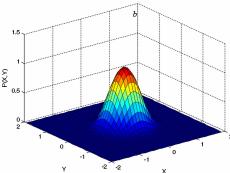
$$\ddot{x} + (b_1 + b_2 \dot{x}^2) \dot{x} + cD^{\alpha} x(t) + \omega_0^2 x + (a_1 x_{\tau} + a_2 \dot{x}_{\tau})$$

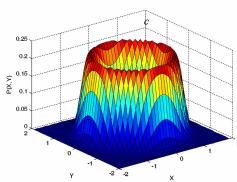
$$= W(t)$$
(33)

其中 c 为分数阶阻尼项的系数, W(t) 为强度 2D 的高斯白噪声. 系统可化为:

$$\ddot{x} + (b_1 + \beta + b_2 \dot{x}^2) \dot{x} + cD^{\alpha} x(t) + \omega^2 x = W(t)$$
 (34)







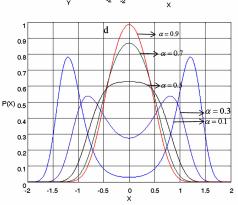


图 3 当 α 改变时的稳态概率密度

Fig. 3 Stationary probability density with variation of α

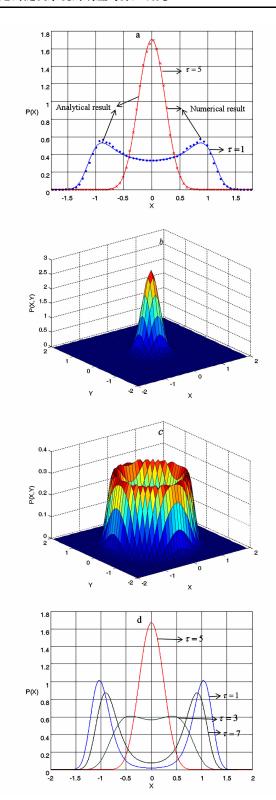


图 4 当 τ 改变时的稳态概率密度

Fig. 4 Stationary probability density with different values of au \ddagger $\dot{\tau}$,

$$\beta = a_2 \cos \omega_0 \tau - \frac{a_1}{\omega_0} \sin \omega_0 \tau \tag{35a}$$

$$\omega^{2} = \omega_{0}^{2} + a_{1}\cos\omega_{0}\tau + a_{2}\omega_{0}\sin\omega_{0}\tau$$
 (35b)
漂移系数和扩散系数分别为:

$$m(A) = -\frac{c\sin(\frac{\alpha\pi}{2})A}{2\omega^{1-\alpha}} - \frac{(\beta + b_1)A}{2} - \frac{3b_2\omega^2A^3}{8} + \frac{D}{2\omega^2A}$$
(36a)

$$\sigma^2(A) = \frac{D}{\omega^2} \tag{36b}$$

由此可导出关于位移速度的联合概率密度、关于位移的概率密度以及关于速度的概率密度.

根据上述计算结果进行模拟. 这里讨论当分数 阶阶数 α 和时滞反馈力发生改变时,系统的变化. 图 3 为当不考虑反馈时滞力的影响时,取不同的分数阶阶数 α 时系统的概率密度,取系统参数分别为:c=0.1,D=0.006, $\omega_0=1.0$, $b_1=-0.07$, $b_2=0.05$. 通过图 3,我们可以清晰地看到 α 的改变可以引起随机分叉现象. 当 $\alpha=0.9$ 时,系统的概率密度图为单峰状态,当 $\alpha=0.1$ 时则为双峰. 故 $\alpha=0.9$ 到 $\alpha=0.1$ 变化的过程中,联合密度由单峰变为火山口形状,系统发生了分叉. 为了更清晰地看到这一过程,图 3(d)为联合概率密度在 $\alpha=0$ 的截面.

图 4 为当时滞反馈控制力发生变化时,系统的 稳态概率密度图,其中参数分别为 $c=0.1,\alpha=0.5$,D=0.006, $\omega_0=1.0$, $a_1=0.1$, $a_2=0$, $b_1=-0.07$, $b_2=0.1$.同样的,我们可以看到随着参数的改变,系统产生了随机分叉现象.

5 结论

本文利用了小时滞项的近似展开和基于广义 谐和函数的随机平均法,研究了时滞反馈力作用下 具有分数阶导数阻尼的随机系统.并通过数值模 拟,验证了方法的有效性.更重点讨论了分数阶阻 尼项以及反馈时滞力对系统响应的影响,可以知道 取不同的分数阶阻尼和反馈时滞力可以改变系统 的概率密度,甚至引起分叉现象.这一结果具有一 定的理论及现实意义.

参考文献

- Machado J T, Kiryakova V, Mainardi F. Recent history of fractional calculus. Communications in Nonlinear Science and Numerical Simulation, 2011, 16 (3): 1140 ~ 1153
- 2 Cafagna D. Past and present-fractional calculus: a mathe-

- matical tool from the past for present engineers. *IEEE Industrial Electronics Magazine*, $2007,1(2):35 \sim 40$
- Bagley R L, Torvik P J. Fractional calculus in the transient analysis of viscoelastically damped structures. AIAA Journal, 2012,23(6):918~925
- 4 Bagley R L, Torvik J. Fractional calculus——A different approach to the analysis of viscoelastically damped structures. AIAA Journal, 2012,21(5):741 ~748
- Bagley R L, Torvik P J. A theoretical basis for the application of fractional calculus to viscoelasticity. *Journal of Rheology*, 1983,27(3):201~210
- 6 Metzler Q, Klafter J. The random walk's guide to anomalous diffusion: a fractional dynamics approach. *Physics Reports*, 200,339(1):1~77
- 7 Agrawal O P. Stochastic analysis of dynamic systems containing fractional derivatives. *Journal of Sound and Vibration*, 2001,247(5):927~938
- 8 Agrawal O P. Stochastic Analysis of a 1-D System With Fractional Damping of Order 1/2. *Journal of Vibration* and Acoustics, 2002,124(3):454 ~ 460
- Spanos P D, Zeldin B A. Random vibration of systems with frequency-dependent parameters or fractional derivatives. *Journal of Engineering Mechanics*, 1997,123(3): 290~292
- Huang Z L, Jin X L. Response and stability of a SDOF strongly nonlinear stochastic system with light damping modeled by a fractional derivative. *Journal of Sound and Vibration*, 2009,319(3):1121~1135
- 11 Chen L C, Zhu W Q. Stochastic jump and bifurcation of Duffing oscillator with fractional derivative damping under combined harmonic and white noise excitations. *Interna*tional Journal of Non-Linear Mechanics, 2011,46 (10): 1324 ~ 1329
- 12 陈林聪,李海锋,李钟慎,朱位秋. 宽带噪声激励下含分数阶导数的 Duffing-Van Del Pol 振子的稳态响应. 西南交通大学学报, 2014,49(1):45~51 (Chen L C, Li H F, Li Z S, Zhu W Q. Relability of Van Der Pol-Duffing oscillator with fractional derivative under wide-bandnoiseexcitations Journal of Southwest Jiaotong University, 2014,49(1):45~51 (in Chinese))
- 13 陈林聪,朱位秋. 谐和与宽带噪声联合激励下含分数导数型阻尼的 Duffing 振子的平稳响应. 应用力学学报, 2010,27(3):517~521 (Chen L C, Zhu W Q. Stationary response of Duffng oscillator with fractional derivative damping under combined harmonic and wide band

- noise xcitations. Chinese Journal of Applied Mechanics, 2010,27(3):517 ~521 (in Chinese))
- 14 Guillouzic S, L'Heureux I, Longtin A. Small delay approximation of stochastic delay differential equations. Physical Review E, 1999,59:3970 ~3982
- 15 Frank T D, Beek P J. Stationary solutions of linear stochastic delay differential equations: Applications to biological systems. *Physical Review E*, 2001,64:021917
- 16 Liu Z H, Zhu W Q. Stochastic averaging of quasi-integrable Hamiltonian systems with delayed feedback control.

- Journal of Sound and Vibration, 2007, 299 (1-2):178 ~ 195
- 17 Xu Z, Cheng Y K. Averaging Method Using Generalized Harmonic Functions For Strongly Non-Linear Oscillators.

 Journal of Sound and Vibration, 1994, 174 (4): 563 ~ 576
- 18 Khasminskii R Z. On an averaging principle for Ito stochastic differential equations. *Kybernetika*, 1968,4:260 ~279 (in Russian)

RESPONSE AND BIFURCATION OF FRACTIONAL STOCHASTIC SYSTEMS WITH TIME-DELAYED FEEDBACK CONTROL*

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Abstract In this paper, the response and bifurcation of fractional stochastic systems with time-delayed feedback control are investigated. We decompose the time-delayed items and apply the stochastic averaging method with the generalized harmonic functions to obtain the stationary response. The effectiveness of the method is verified by two different examples. The simulation results show that different system parameters can affect the response of the system, and it can induce the occurrence of stochastic bifurcation for some certain systems as well.

Key words time-delayed, fractional, stochastic system, stochastic averaging method, stochastic bifurcation

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